Trapezoidal screws type KRE

A2 stainless steel - AISI 304 1.4301

Stock no. for screw **RIGHT**	Stock no. for screw **LEFT**	**Diameter x lead**	Thread starts	Lead accuracy µm /300 mm	Straightness mm / mm	Weight kg/mt
■ KRE 08 A R …	□ KRE 08 A L …	**Tr 8x1,5**	1	200	1,5 / 300	0,30
■ KRE 10 T R …	■ KRE 10 T L …	**Tr 10x2**	1	200	1,5 / 300	0,48
■ KRE 10 A R …	■ KRE 10 A L …	**Tr 10x3**	1	200	1,5 / 300	0,42
■ KRE 12 A R …	■ KRE 12 A L …	**Tr 12x3**	1	200	1,5 / 300	0,65
□ KRE 14 R R …	□ KRE 14 R L …	**Tr 14x3**	1	200	1,5 / 300	0,93
■ KRE 14 A R …	■ KRE 14 A L …	**Tr 14x4**	1	200	1,5 / 300	0,86
■ KRE 16 A R …	■ KRE 16 A L …	**Tr 16x4**	1	200	1,5 / 300	1,17
■ KRE 18 A R …	■ KRE 18 A L …	**Tr 18x4**	1	200	1,5 / 300	1,53
■ KRE 20 A R …	■ KRE 20 A L …	**Tr 20x4**	1	200	1,5 / 300	1,94
□ KRE 22 A R …	□ KRE 22 A L …	**Tr 22x5**	1	200	1,5 / 300	2,29
■ KRE 24 A R …	■ KRE 24 A L …	**Tr 24x5**	1	200	1,5 / 300	2,78
■ KRE 25 A R …	■ KRE 25 A L …	**Tr 25x5**	1	200	1,5 / 300	3,05
■ KRE 26 A R …	□ KRE 26 A L …	**Tr 26x5**	1	200	1,5 / 300	3,33
■ KRE 28 A R …	□ KRE 28 A L …	**Tr 28x5**	1	200	1,5 / 300	3,92
□ KRE 30 P R …	□ KRE 30 P L …	**Tr 30x5**	1	200	1,5 / 300	4,57
■ KRE 30 A R …	■ KRE 30 A L …	**Tr 30x6**	1	200	1,5 / 300	4,38
□ KRE 32 A R …	□ KRE 32 A L …	**Tr 32x6**	1	200	1,5 / 300	5,06
□ KRE 35 P R …	□ KRE 35 P L …	**Tr 35x5**	1	200	1,5 / 300	6,40
■ KRE 35 A R …	■ KRE 35 A L …	**Tr 35x6**	1	200	1,5 / 300	6,16
■ KRE 36 A R …	■ KRE 36 A L …	**Tr 36x6**	1	200	1,5 / 300	6,56
□ KRE 40 P R …	□ KRE 40 P L …	**Tr 40x5**	1	200	1,5 / 300	8,51
□ KRE 40 O R …	□ KRE 40 O L …	**Tr 40x6**	1	200	1,5 / 300	8,26
■ KRE 40 A R …	■ KRE 40 A L …	**Tr 40x7**	1	200	1,5 / 300	8,03
□ KRE 44 A R …	□ KRE 44 A L …	**Tr 44x7**	1	200	1,5 / 300	9,90
□ KRE 50 P R …	□ KRE 50 P L …	**Tr 50x5**	1	200	1,5 / 300	13,70
□ KRE 50 O R …	□ KRE 50 O L …	**Tr 50x6**	1	200	1,5 / 300	13,35
■ KRE 50 A R …	■ KRE 50 A L …	**Tr 50x8**	1	200	1,5 / 300	12,90
□ KRE 55 A R …	□ KRE 55 A L …	**Tr 55x9**	1	200	1,5 / 300	15,51
□ KRE 60 O R …	□ KRE 60 O L …	**Tr 60x6**	1	200	1,5 / 300	19,67
□ KRE 60 N R …	□ KRE 60 N L …	**Tr 60x7**	1	200	1,5 / 300	19,36
■ KRE 60 A R …	■ KRE 60 A L …	**Tr 60x9**	1	200	1,5 / 300	18,74
■ KRE 70 A R …	■ KRE 70 A L …	**Tr 70x10**	1	200	1,5 / 300	25,80
■ KRE 80 A R …	■ KRE 80 A L …	**Tr 80x10**	1	200	1,5 / 300	34,39
■ KRE 90 A R …	■ KRE 90 A L …	**Tr 90x12**	1	200	1,5 / 300	43,07
□ KRE A0 A R …	□ KRE A0 A L …	**Tr 100x12**	1	200	1,5 / 300	53,99

■ = Goods in stock. □ = Goods available upon request only.

Trapezoidal screws type KRP
A2 stainless steel - AISI 304 1.4301

Stock no. for screw **RIGHT**	Stock no. for screw **LEFT**	**Diameter x lead**	Thread starts	Lead accuracy µm /300 mm	Straightness mm / mm	Weight kg/mt
□ KRP 10 J R …	□ KRP 10 J L …	**Tr 10x4 (P2)**	2	200	0,7 / 1000	0,48
■ KRP 12 B R …	□ KRP 12 B L …	**Tr 12x6 (P3)**	2	200	0,7 / 1000	0,65
□ KRP 14 B R …	□ KRP 14 B L …	**Tr 14x6 (P3)**	2	200	0,7 / 1000	0,93
■ KRP 16 B R …	□ KRP 16 B L …	**Tr 16x8 (P4)**	2	200	0,7 / 1500	1,17
□ KRP 18 B R …	□ KRP 18 B L …	**Tr 18x8 (P4)**	2	200	0,7 / 1500	1,53
■ KRP 20 B R …	□ KRP 20 B L …	**Tr 20x8 (P4)**	2	200	0,6 / 2000	1,94
□ KRP 20 E R …	□ KRP 20 E L …	**Tr 20x20 (P4)**	5	200	0,4 / 2000	1,94
□ KRP 20 D R …	□ KRP 20 D L …	**Tr 20x20 (P5)**	4	200	0,4 / 2000	1,84
□ KRP 22 B R …	□ KRP 22 B L …	**Tr 22x10 (P5)**	2	200	0,4 / 2000	2,29
■ KRP 24 B R …	□ KRP 24 B L …	**Tr 24x10 (P5)**	2	200	0,4 / 2000	2,78
■ KRP 25 B R …	□ KRP 25 B L …	**Tr 25x10 (P5)**	2	200	0,4 / 2000	3,05
□ KRP 26 B R …	□ KRP 26 B L …	**Tr 26x10 (P5)**	2	200	0,4 / 2000	3,33
□ KRP 28 B R …	□ KRP 28 B L …	**Tr 28x10 (P5)**	2	200	0,4 / 2000	3,92
■ KRP 30 B R …	□ KRP 30 B L …	**Tr 30x12 (P6)**	2	200	0,4 / 3000	4,38
□ KRP 32 B R …	□ KRP 32 B L …	**Tr 32x12 (P6)**	2	200	0,4 / 3000	5,06
□ KRP 36 B R …	□ KRP 36 B L …	**Tr 36x12 (P6)**	2	200	0,3 / 3000	6,56
■ KRP 40 B R …	□ KRP 40 B L …	**Tr 40x14 (P7)**	2	200	0,3 / 3000	8,03

■ = Goods in stock. □ = Goods available upon request only.

Trapezoidal screws type KRE
A2 stainless steel - AISI 304 1.4301

Stock no. for screw **RIGHT**	Stock no. for screw **LEFT**	**Diameter x lead**	Thread starts	Lead accuracy µm /300 mm	Straightness mm / mm	Weight kg/mt
□ KRE 10 J R …	□ KRE 10 J L …	**Tr 10x4 (P2)**	2	200	1,5 / 300	0,48
■ KRE 12 B R …	□ KRE 12 B L …	**Tr 12x6 (P3)**	2	200	1,5 / 300	0,65
□ KRE 14 B R …	□ KRE 14 B L …	**Tr 14x6 (P3)**	2	200	1,5 / 300	0,93
■ KRE 16 B R …	□ KRE 16 B L …	**Tr 16x8 (P4)**	2	200	1,5 / 300	1,17
□ KRE 18 B R …	□ KRE 18 B L …	**Tr 18x8 (P4)**	2	200	1,5 / 300	1,53
■ KRE 20 B R …	□ KRE 20 B L …	**Tr 20x8 (P4)**	2	200	1,5 / 300	1,94
□ KRE 20 E R …	□ KRE 20 E L …	**Tr 20x20 (P4)**	5	200	1,5 / 300	1,94
□ KRE 20 D R …	□ KRE 20 D L …	**Tr 20x20 (P5)**	4	200	1,5 / 300	1,84
□ KRE 22 B R …	□ KRE 22 B L …	**Tr 22x10 (P5)**	2	200	1,5 / 300	2,29
■ KRE 24 B R …	□ KRE 24 B L …	**Tr 24x10 (P5)**	2	200	1,5 / 300	2,78
■ KRE 25 B R …	□ KRE 25 B L …	**Tr 25x10 (P5)**	2	200	1,5 / 300	3,05
□ KRE 26 B R …	□ KRE 26 B L …	**Tr 26x10 (P5)**	2	200	1,5 / 300	3,33
□ KRE 28 B R …	□ KRE 28 B L …	**Tr 28x10 (P5)**	2	200	1,5 / 300	3,92
■ KRE 30 B R …	□ KRE 30 B L …	**Tr 30x12 (P6)**	2	200	1,5 / 300	4,38
□ KRE 32 B R …	□ KRE 32 B L …	**Tr 32x12 (P6)**	2	200	1,5 / 300	5,06
□ KRE 36 B R …	□ KRE 36 B L …	**Tr 36x12 (P6)**	2	200	1,5 / 300	6,56
■ KRE 40 B R …	□ KRE 40 B L …	**Tr 40x14 (P7)**	2	200	1,5 / 300	8,03

■ = Goods in stock. □ = Goods available upon request only.

Trapezoidal screw specifications (also see pages for each screw type)

Diameter x lead	d 1 Major diameter tolerance **4 h** mm		d 2 Effective or pitch dia. tolerance **7 e** mm		d 3 Minor diameter tolerance **7 h** mm		Thread starts	Lead angle	(1) Efficiency η		(2) **H 1** mm	**I** Moment of inertia mm^4
	min.	max.	min.	max.	min.	max.			*f*=0.1	*f*=0.2		
Tr 8 x 1,5	7,850	8,000	7,013	7,183	5,921	6,200	1	3°46’	0,39	0,24	1,0	60
Tr 10 x 2	9.820	10.000	8.739	8.929	7.191	7.500	1	4°02’	0.41	0.26	1.0	131
Tr 10 x 3	9.764	10.000	8.203	8.415	6.150	6.500	1	6°25’	0.52	0.35	1.5	70
Tr 10 x 4 (P2)	9.820	10.000	8.739	8.929	7.191	7.500	2	8°03’	0.58	0.40	1.0	131
Tr 12 x 3	11.764	12.000	10.191	10.415	8.135	8.500	1	5°12’	0.47	0.31	1.5	215
Tr 12 x 6 (P3)	11.764	12.000	10.191	10.415	8.135	8.500	2	10°19’	0.63	0.46	1.5	215
Tr 14 x 3	13.764	14.000	12.191	12.415	10.135	10.500	1	4°22’	0.43	0.27	1.5	518
Tr 14 x 4	13.700	14.000	11.640	11.905	9.074	9.500	1	6°03’	0.51	0.34	2.0	333
Tr 14 x 6 (P3)	13.764	14.000	12.191	12.415	10.135	10.500	2	8°41’	0.59	0.42	1.5	518
Tr 16 x 4	15.700	16.000	13.640	13.905	11.074	11.500	1	5°12’	0.47	0.31	2.0	738
Tr 16 x 8 (P4)	15.700	16.000	13.640	13.905	11.074	11.500	2	10°19’	0.63	0.46	2.0	738
Tr 18 x 4	17.700	18.000	15.640	15.905	13.074	13.500	1	4°33’	0.44	0.28	2.0	1434
Tr 18 x 8 (P4)	17.700	18.000	15.640	15.905	13.074	13.500	2	9°02’	0.60	0.43	2.0	1434
Tr 20 x 4	19.700	20.000	17.640	17.905	15.074	15.500	1	4°03’	0.41	0.26	2.0	2534
Tr 20 x 8 (P4)	19.700	20.000	17.640	17.905	15.074	15.500	2	8°03’	0.58	0.40	2.0	2534
Tr 20 x 20 (P4)	19.700	20.000	17.640	17.905	15.074	15.500	5	19°28’	0.75	0.59	2.0	2534
Tr 20 x 20 (P5)	19.665	20.000	17.114	17.394	14.044	14.500	4	20°00’	0.76	0.60	2.5	1910
Tr 22 x 5	21.665	22.000	19.114	19.394	16.044	16.500	1	4°40’	0.45	0.28	2.5	3232
Tr 22 x 10 (P5)	21.665	22.000	19.114	19.394	16.044	16.500	2	9°16’	0.61	0.43	2.5	3232
Tr 24 x 5	23.665	24.000	21.094	21.394	18.019	18.500	1	4°14’	0.42	0.27	2.5	5175
Tr 24 x 10 (P5)	23.665	24.000	21.094	21.394	18.019	18.500	2	8°25’	0.59	0.41	2.5	5175
Tr 25 x 3	24.764	25.000	23.165	23.415	21.103	21.500	1	2°20’	0.29	0.17	1.5	9735
Tr 25 x 5	24.665	25.000	22.094	22.394	19.019	19.500	1	4°03’	0.41	0.26	2.5	6423
Tr 25 x 10 (P5)	24.665	25.000	22.094	22.394	19.019	19.500	2	8°03’	0.58	0.40	2.5	6423
Tr 25 x 25 (P5)	24.665	25.000	22.094	22.394	19.019	19.500	5	19°30’	0.75	0.60	2.5	6423
Tr 26 x 5	25.665	26.000	23.094	23.394	20.019	20.500	1	3°52’	0.40	0.25	2.5	7884
Tr 26 x 10 (P5)	25.665	26.000	23.094	23.394	20.019	20.500	2	7°42’	0.57	0.39	2.5	7884
Tr 28 x 5	27.665	28.000	25.094	25.394	22.019	22.500	1	3°34’	0.38	0.23	2.5	11539
Tr 28 x 10 (P5)	27.665	28.000	25.094	25.394	22.019	22.500	2	7°07’	0.55	0.37	2.5	11539
Tr 30 x 3	29.764	30.000	28.165	28.415	26.103	26.500	1	1°55’	0.25	0.14	1.5	22900
Tr 30 x 4	29.700	30.000	27.640	27.905	25.074	25.500	1	2°36’	0.31	0.18	2.0	19400
Tr 30 x 5	29.665	30.000	27.094	27.394	24.019	24.500	1	3°19’	0.36	0.22	2.5	16340
Tr 30 x 6	29.625	30.000	26.547	26.882	22.463	23.000	1	4°03’	0.41	0.26	3.0	13650
Tr 30 x 12 (P6)	29.625	30.000	26.547	26.882	22.463	23.000	2	8°03’	0.58	0.40	3.0	13650
Tr 30 x 30 (P5)	29.665	30.000	27.094	27.394	24.019	24.500	6	19°09’	0.75	0.59	2.5	16340
Tr 32 x 6	31.625	32.000	28.547	28.882	24.463	25.000	1	3°46’	0.39	0.24	3.0	17580
Tr 32 x 12 (P6)	31.625	32.000	28.547	28.882	24.463	25.000	2	7°30’	0.56	0.38	3.0	17580
Tr 35 x 3	34.764	35.000	33.165	33.415	31.103	31.500	1	1°38’	0.22	0.12	1.5	46128
Tr 35 x 4	34.700	35.000	32.640	32.905	30.074	30.500	1	2°13’	0.28	0.16	2.0	40150
Tr 35 x 5	34.665	35.000	32.094	32.394	29.019	29.500	1	2°48’	0.33	0.19	2.5	34810
Tr 35 x 6	34.625	35.000	31.547	31.882	27.463	28.000	1	3°25’	0.37	0.23	3.0	30000
Tr 35 x 8	34.550	35.000	30.493	30.868	25.399	26.000	1	4°42’	0.45	0.29	4.0	21980
Tr 36 x 6	35.625	36.000	32.547	32.882	28.463	29.000	1	3°19’	0.36	0.22	3.0	34540
Tr 36 x 12 (P6)	35.625	36.000	32.547	32.882	28.463	29.000	2	6°36’	0.53	0.36	3.0	34540

(1) Useful effect for conversion of rotary motion into linear motion with friction *f* =0.1 and *f* =0.2.

(2) Radial support dimension between screw and nut teeth.

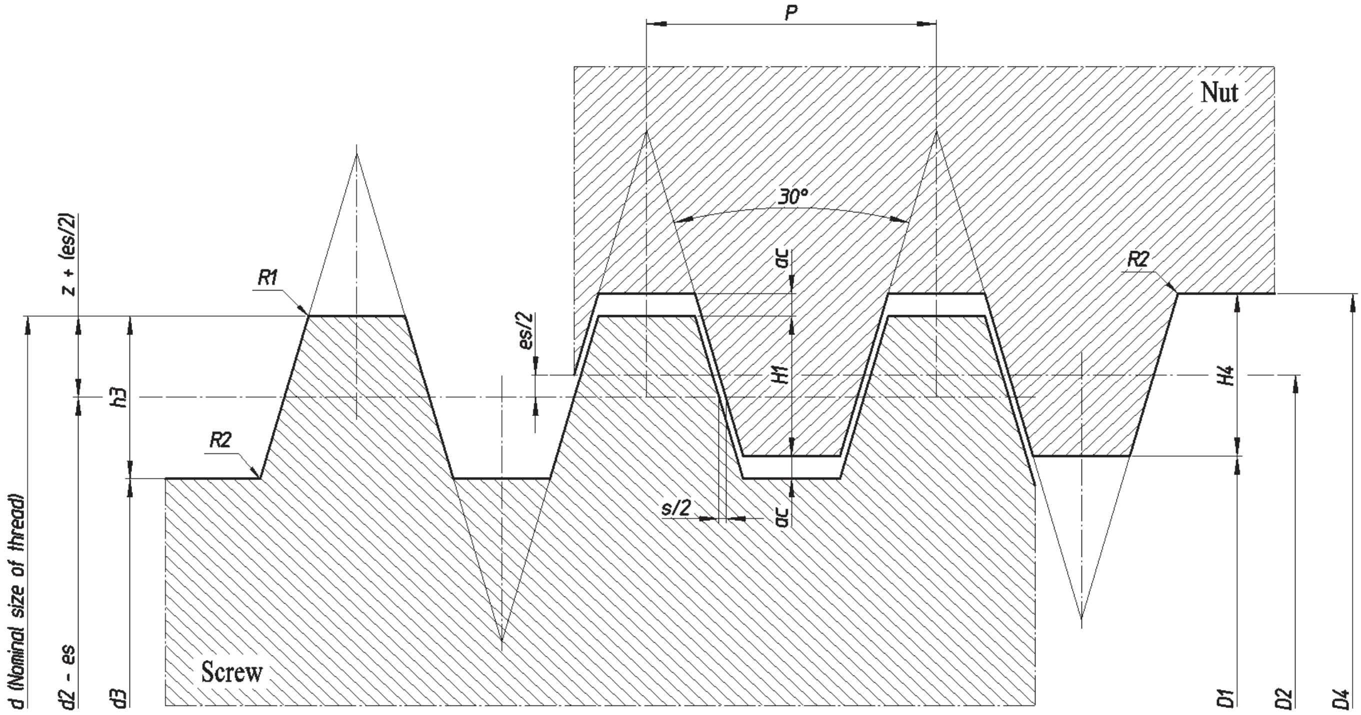
Trapezoidal screw specifications (also see pages for each screw type)

Diameter x lead	d 1 Major diameter tolerance **4 h** min.	max. mm	d 2 Effective or pitch dia. tolerance **7 e** min.	max. mm	d 3 Minor diameter tolerance **7 h** min.	max. mm	Thread starts	Lead angle	(1) Efficiency η f=0.1	f=0.2	(2) **H 1** mm	**I** Moment of inertia mm^4
Tr 40 x 3	39.764	40.000	38.165	38.415	36.103	36.500	1	1°25’	0.20	0.11	1.5	83395
Tr 40 x 4	39.700	40.000	37.640	37.905	35.074	35.500	1	1°55’	0.25	0.14	2.0	74290
Tr 40 x 5	39.665	40.000	37.094	37.394	34.019	34.500	1	2°26’	0.30	0.17	2.5	65740
Tr 40 x 6	39.625	40.000	36.547	36.882	32.463	33.000	1	2°57’	0.34	0.20	3.0	57950
Tr 40 x 7	39.575	40.000	36.020	36.375	31.431	32.000	1	3°30’	0.38	0.23	3.5	51030
Tr 40 x 8	39.550	40.000	35.493	35.868	30.399	31.000	1	4°03’	0.41	0.26	4.0	44560
Tr 40 x 10	39.470	40.000	34.450	34.850	28.350	29.000	1	5°12’	0.47	0.31	5.0	31700
Tr 40 x 14 (P7)	39.575	40.000	36.020	36.375	31.431	32.000	2	6°58’	0.54	0.37	3.5	51030
Tr 40 x 40 (P8)	39.550	40.000	35.493	35.868	30.399	31.000	5	19°30’	0.75	0.60	4.0	44560
Tr 44 x 7	43.575	44.000	40.020	40.375	35.431	36.000	1	3°09’	0.35	0.21	3.5	81820
Tr 45 x 8	44.550	45.000	40.493	40.868	35.399	36.000	1	3°33’	0.38	0.23	4.0	81245
Tr 50 x 3	49.764	50.000	48.150	48.415	46.084	46.500	1	1°08’	0.16	0.09	1.5	121400
Tr 50 x 4	49.700	50.000	47.605	47.905	45.074	45.500	1	1°31’	0.21	0.12	2.0	202600
Tr 50 x 5	49.665	50.000	47.094	47.394	44.019	44.500	1	1°55’	0.25	0.14	2.5	184300
Tr 50 x 6	49.625	50.000	46.547	46.882	42.463	43.000	1	2°20’	0.29	0.17	3.0	167240
Tr 50 x 8	49.550	50.000	45.468	45.868	40.368	41.000	1	3°10’	0.35	0.21	4.0	136930
Tr 50 x 10	49.470	50.000	44.425	44.850	38.319	39.000	1	4°03’	0.41	0.26	5.0	105834
Tr 55 x 9	54.500	55.000	49.935	50.360	44.329	45.000	1	3°15’	0.36	0.22	4.5	189550
Tr 60 x 6	59.625	60.000	56.547	56.882	52.463	53.000	1	1°55’	0.25	0.14	3.0	386240
Tr 60 x 7	59.575	60.000	56.020	56.375	51.431	52.000	1	2°16’	0.28	0.16	3.5	343450
Tr 60 x 9	59.500	60.000	54.935	55.360	49.329	50.000	1	2°57’	0.34	0.20	4.5	302600
Tr 70 x 10	69.470	70.000	64.425	64.850	58.319	59.000	1	2°48’	0.33	0.19	5.0	587540
Tr 80 x 10	79.470	80.000	74.425	74.850	68.319	69.000	1	2°26’	0.30	0.17	5.0	1069390
Tr 90 x 12	89.400	90.000	83.335	83.830	76.246	77.000	1	2°36’	0.31	0.18	6.0	1658969
Tr 95 x 16	94.290	95.000	86.250	86.810	76.110	77.000	1	3°21’	0.37	0.22	8.0	1647164
Tr 100 x 12	99.400	100.000	93.330	93.830	86.215	87.000	1	2°19’	0.29	0.17	6.0	2712072
Tr 100 x 16	99.290	100.000	91.250	91.810	81.110	82.000	1	3°10’	0.35	0.21	8.0	2124553
Tr 120 x 14	119.330	120.000	112.290	112.820	103.157	104.00	1	2°16’	0.28	0.16	7.0	5558591
Tr 120 x 16	119.290	120.000	111.250	111.810	101.110	102.00	1	2°36’	0.31	0.16	8.0	5130342
Tr 140 x 14	139.330	140.000	132.290	132.820	123.157	124.00	1	1°55’	0.25	0.14	7.0	11292921
Tr 160 x 16	159.290	160.000	151.250	151.810	141.110	142.00	1	1°55’	0.25	0.14	8.0	19462609

(1) Useful effect for conversion of rotary motion into linear motion with friction f =0.1 and f =0.2.

(2) Radial support dimension between screw and nut teeth.

PROFILE FOR METRIC TRAPEZOIDAL THREADS TO ISO STANDARD 2901 – 2902 – 2903 – 2904



$H_1 = 0,5\ P$
$h_3 = H_4 = H_1 + a_c = 0.5\ P + ac$
$z = 0,25\ P = H_1/2$
$d_3 = d - 2\ h_3$
$d_2 = D_2 = d - 2\ z = d - 0.5\ P$
$D_2 = d + 2\ a_c$
a_c = bottom play
es = top deviation for screw
s = 0,26795 es
R_1 max. = 0.5 a_c
R_2 max. = a_c

Sizes stocked. Ready reference:

 We riserve the right to change sizes and features without notice.

Features of CONTI Trapezoidal Screws and Nuts

CONTI trapezoidal screws are precision rolled. Continuous search for improvement and many years of CONTI experience in the development of the cold plastic deformation process which characterizes rolling allow us to offer our customers trapezoidal screws with excellent features.

Materials

Steel used in trapezoidal screws:		**Surface hardness after rolling**
EN 10084 C15E - 1.1141	carbon steel	App. 160/180 HB
EN 10083-2 1C45 - 1.0503	carbon steel	App. 250 HB
Inox A2 - AISI 304 -1.4301	stainless steel	App. 260 HB
Inox A4 - AISI 316 - 1.4401	stainless steel	App. 280 HB

C45 and A2 stainless steel were chosen because in addition to their natural qualities as good construction materials, after rolling they give very good surface hardness and finish on the thread sides. A4 stainless steel also has excellent corrosion resistance. C15 is an excellent quality-price compromise.
Roughness is less than 1 µm Ra for all.
These two features are decisive factors for qualitative appraisal of trapezoidal screws because they give very small friction coefficients, much lower than those obtainable with machined screws where other conditions such as speed, load and lubrication are equal.
Our trapezoidal screws coupled with bronze nuts give the opportunity to realize translation systems whose efficiency, flowability and quietness are much lower comparing to a coupling with machined screws.
Because of the low friction coefficient the amount of heat generated during movement is limited with resulting smaller nut heating. Nut life is also increased. We make nuts with 10 kinds of material to better meet the various requirements.

Steel used in nuts:

EN 10277-3 11SMnPb37 – 1.0737	steel with sulphur, manganese and lead
INOX A1- AISI 303 – 1.4305	stainless steel

Brass used in nuts:

EN 12164 CW614N-M	brass

Bronze used in nuts:

EN 1982 CuSn5Zn5Pb5-C – CC491K	tin bronze with zinc and lead	60-70 HB
EN 1982 CuSn7Zn4Pb7-C – CC493K	tin bronze with zinc and lead	65-75 HB
EN 1982 CuSn12-C – CC483K	tin bronze	80-100 HB
EN 1982 CuAl11Fe6Ni6-C – CC483K	aluminium bronze	160-220 HB

Plastic used in nuts:

PA 6 + Mo S2 DIN 7728	plastic
PA 6 + Mo S2 DIN 7728 + additives	self-lubricating plastic

The nuts we make with length 3xTr: HDL, BIG and HAL deserve special attention.
These bronze nuts, thanks to their considerable length, distribute the load over a larger number of holding threads and this limit surface contact pressure between screw and nut. This is decisive for long nut life.
By using the 3xTr long nuts compared with bronze nuts with conventional length (approximately 1.5xTr or 2xTr), very high loads can be withstood for equal traversing speed.
In particular, with HAL aluminium bronze nuts very high loads can be born and it is recommended to apply continuous steady lubrication. HAL nuts have to be coupled with screws in C45 or in stainless steel A2 or A4; C15 screws are not recommended.
Where it is not desired to lubricate trapezoidal screws, self-lubricating plastic nuts are recommended.
It is not possible to couple plastic nuts with screws made by machining.

Positioning Accuracy

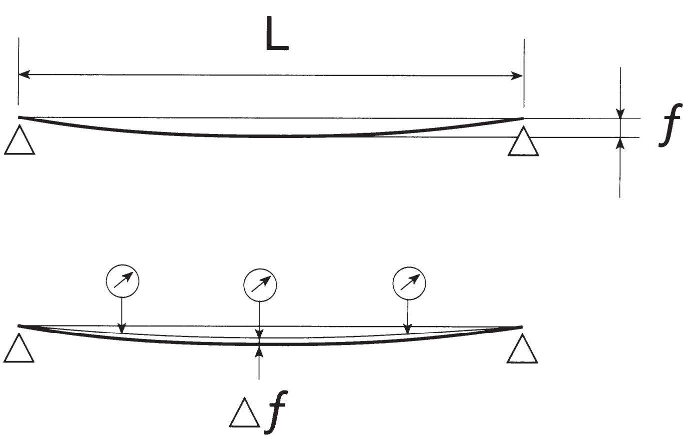
To better meet the requirements of customers using trapezoidal screws as positioning system we produce screws with lead accuracy according to the following table

Screw type	Lead Accuracy	Pitch error
KTS	100 (200 *)	+/- 0.100 mm every 300 mm of thread
KUE	100 (200 *)	+/- 0.100 mm every 300 mm of thread
KKA	50	+/- 0.050 mm every 300 mm of thread
KSR	500	+/- 0.500 mm every 300 mm of thread
KQX	200	+/- 0.200 mm every 300 mm of thread
KEQ	200	+/- 0.200 mm every 300 mm of thread
KRP	200	+/- 0.200 mm every 300 mm of thread
KRE	200	+/- 0.200 mm every 300 mm of thread
KAM	200	+/- 0.200 mm every 300 mm of thread
KAF	200	+/- 0.200 mm every 300 mm of thread

* Class 200 for diameters bigger than 80x10.

Straightness

CONTI screws are produced with controlled straightness.
Screw straightness is appraised by measuring the variation of the deflection "*f*" when the screw is supported at the ends on two constraints and slightly rotated.
For example, the screw KKA Tr 30 A (threading Tr 30 x 6 with 1 start) has straightness error of max 0.3 on 3000 mm.
This means that a screw Tr 30x6 3000 mm long resting on two constraints at the ends and rotated slightly displays a camber variation "Δf " less than 0.3 mm at all points of the screw.



f = screw weight camber

for screws Tr 30x6 with L = 3000 mm
Δf maximum: 0.3 mm

Good screw straightness gives operation with load always centred on the axis, hence uniform distribution of surface contact pressure between screw and nut with resulting smooth running, and regular rotation and translation.

General choice criteria

The choice between different types of available screws and nuts is generally made considering the following:

Choice of the screw

Working environment

For work environments where there are no particular corrosive or oxidizing agents C45 screws can be used. Where these conditions are not met, we recommend using stainless steel screws A2 or A4 which are particularly suitable in the following cases:

- With relative humidity of 70/80% and above.
- Immersed in water, even in sea water.
- In presence of particular corrosive agents such as chlorides. In case of highly corrosive agents please contact our Technical Department.
- Where, due to special construction requirements, components must not oxidise, for example in the food industry, where they are coupled with nuts HDA.
- Where the screws cannot be reached for lubrication. For "maintenance free" constructions they are mainly coupled with self-lubricating plastic nuts.
- Where working temperature is relatively high because the stainless steel A2 and A4 feature a relatively high slag temperature due to the austenitic structure of the material.

Positioning accuracy

For positioning screws it is necessary to have the control of the error of the thread pitch. We provide customer screws with accuracy class 50 (50 µm/300 mm), 100 (100 µm/300 mm) and screws with class 200 (200 µm/300 mm) both in C45 and stainless steel A2. For standard carriage lead screws class 200 ones can be used.

Irreversibility

The complete irreversibility occurs with trapezoidal screw with helix angle < 2° 30'.
In all other cases, torque may be transmitted to the drive gear in a still screw condition subject to a load on the nut (especially under vibration). However, a good irreversibility is present up to 5 or 6 degrees.

Choice of the nut

Working environment

The available materials used for the production of nuts, both in bronze and stainless steel 303, are resistant to most of the oxidizing agents that occur in various applications of the trapezoidal screw/nut system. In presence of corrosive agents please contact our Technical Department.

In applications where the presence of added lubricants (grease or oil) is not allowed, we recommend to use self lubricating plastic nuts.

The use of plastics is restrained by the actual working conditions, therefore you may need to study the solution together with our technical department, and not rely on a choice based on intuition only. This because plastics have sometimes excellent self-lubrication features, but have, at the same time, restrictions on the working temperature or humidity absorption problems, as well as some mechanical properties that may not be suitable for the intended use. The preliminary study of the application, in such cases, is therefore required to achieve positive and satisfying results.

General sizing criteria

The actual sizing of a trapezoidal screw/nut system has to be done considering the following three points:

1. sizing to wear
2. sizing the critical bending load
3. sizing to the critical speed

In order to obtain a good working condition of a screw/nut system, all three above mentioned points must be respected when sizing.

Sizing to wear

The coupling screw/nut system has been used for a long time in a lot of applications to convert rotary motion into linear motion. The total power applied to the screw (Pt) is transformed into usable power (Pu) on the nut. The ratio Pu / Pt = η defines the efficiency of the system, which basically depends on the friction coefficient between the contacting surfaces of the screw and the nut, as well as on the lead angle. Because of the presence of sliding friction, part of the power is converted into heat. Just looking into this sliding friction, parameters can be given to evaluate the functioning of the system. The criterion is to limit the contact surface pressure on the side of the thread to allow a smooth glide between the two surfaces to avoid therefore heavy friction that erodes the nut. The product p ● Vst must be also limited (p = contact surface pressure and Vst = sliding speed on the effective diameter of the thread) in order to reduce the power that is dissipated into heat. This helps to reduce the temperature of the surfaces in contact. This limitation is important to avoid lubricant damages if bronze nuts are used. In case of use of self-lubricating plastic nuts, without the addition of further oil or grease, temperature should be checked as at higher temperatures the values of the product p ● Vst must be kept at low values.

Calculation of the contact surface pressure "p"

The contact surface pressure "p" is calculated using the following formula:

(1) $$p = \frac{F}{At}$$

F = Axial Force [N]
At = Total bearing surface between the teeth of the nut and the screw in the plane perpendicular to the axis. [mm^2]

(2) $$At = \pi \bullet dm \bullet Z \bullet H1$$

dm = mean diameter of the thread [mm]
H1 = support radial size between the teeth of the screw and the nut [mm]
Z = n° of gripping teeth

$$Z = \frac{h\ nut\ [mm]}{\left(\frac{real\text{ - }pitch\ [mm]}{n°\ starts}\right)}$$

For standard nuts each At value has been reported into the tables.

Calculation of the sliding speed "Vst"

The sliding speed is calculated using one of the following formulas:

- if round speed of the screw has already been defined:

(3) $$Vst = \frac{n \bullet P}{1000 \bullet sen\ \alpha}$$

n = RPM $\left[\frac{round}{min.}\right]$
P = thread pitch [mm]
α = thread helix angle

- if we have already established at which speed the nut must move:

(4) $$Vst = \frac{Vtr}{sen\alpha}$$

Vst = sliding speed on mean diametre. [m/min]
Vtr = motion speed [m/min]
α = thread helix angle

Please note that the screw RPM and the motion speed are bound as follows:

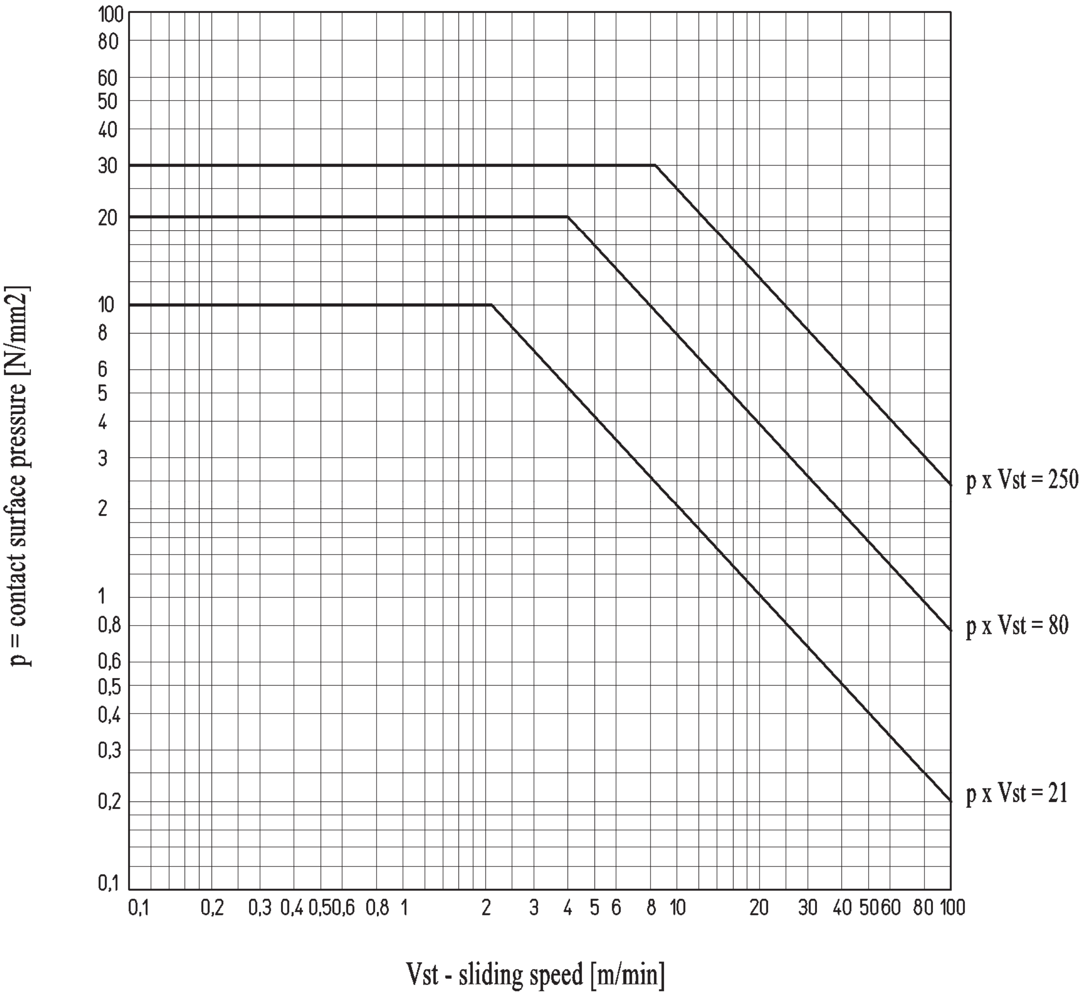
(5) $$n = \frac{1000 \bullet Vtr}{P}$$

n = RPM
Vtr = motion speed [m/min]
P = thread pitch [mm]

Bronze nut sizing

As per the bronze nut, the study of the product p•Vst allows you to plot the graph N.1 where three areas are highlighted, each of which is characterized by certain working conditions that in terms of smoothness of the surfaces in contact allow us to make evaluations based on experimental results previously obtained. A good lubrication is always necessary, possibly with oil. With little or no lubrication working condition may vary greatly.

Graph N° 1 – Sliding condition for Bronze



Area A : area A is enclosed by the limit p•Vst = 21 [N/mm^2 • m/min]
In this area, the operation is in the best conditions.
"Continuous service" is possible as the amount of heat produced within these limits p ● Vst is pretty low. Therefore the life of the nut is very good.

Area B : area B is enclosed by the limit p•Vst = 80 [N/mm^2 • m/min]
In this area, the operation is in more severe conditions.
In such conditions a steady lubrication is required to contain the erosion of the bronze nut in order to still have a good lifetime. “Continuous service” is possible for limited periods only, as the amount of heat that is produced may lead to the overheating of the nut. It also depends on the real amount of oil used because, beside the lubrication, it helps reducing the heat. The life of the nut is however limited.

Area C : area C is enclosed by the limit p•Vst = 250 [N/mm^2 • m/min]
In this area, the operation is in very heavy conditions.
With these values of p•Vst “continuous service” is certainly not possible. Even with good lubrication we face a great overheating and a very quick nut wear off, because the fiction between the surfaces in contact causes a rapid erosion of the nut.

General considerations for bronze nuts

In all three working conditions described, the bronze nut wear off is greatly affected by the real lubricating condition during operation. Giving acceptable reference values is therefore impossible during the project of the life of the nut. Pay particular attention to those applications where working room temperature is above l40/150°C, as such temperatures may damage the lubricant with consequent deterioration of operating conditions and lifetime. In such cases we recommend the use of lubricants designed to withstand high temperatures.

Safety factor for the forces of inertia "*f i*"

During the sizing process we must also check that the inertia forces present during acceleration and deceleration are relatively low so that the value of p●Vst remains within the controlled limits. Whereas this calculation is difficult, in the presence of a non-uniform movement or under great variations, safety factors reported in Chart. N°1 must be considered.

Chart. N° 1: Safety factors with respect to the forces of inertia

Load Type	*f i*
Constant loads and controlled acceleration / deceleration.	from l to 0,5
Constant loads and violent start and stop	from 0,5 to 0,33
Loads and speed greatly variable	from 0,33 to 0,25
Loads in presence of shocks and vibrations	from 0,25 to 0,17

The coefficient "*f i*" is used to correct the value of the product " $(p \bullet Vst)_{max}$" derived from the graph N° 1, considering the maximum admissible sliding speed to the value of the contact surface pressure related to the real case in exam. Working "area" limits (A, B or C) must be considered.
To calculate p•Vst related to the case in exam admissible the following **(6)** must be used

$$\textbf{(6)} \quad p \bullet Vst\ am = (p \bullet Vst)_{max} \bullet f\,i$$

Example of calculation with bronze nut

Size to wear a bronze nut which must operate in continuous service remaining within the maximum limit value of p•Vst = 21 (Area A), with good lubrication.
Constant axial load without relevant variations, with forces of inertia limited by controlled ramps of acceleration/deceleration.

Axial load F = 1200 N (1 Kg*f* = 9,81N)
Constant motion speed Vtr = 2, 8 m/min
Evaluation of the product p•Vst using a nut FTN 30 AR (bronze flanged nut with thread Tr 30x6 1 start, right)

Contact surface pressure is calculated with **(1)** (see page 57)

$$p = \frac{F}{At} = \frac{1200\,[N]}{2120\,[mm^2]} = 0{,}57 \left[\frac{N}{mm^2}\right]$$

F = Axial Force [N]
At = Total bearing surface between the teeth of the screws and the nuts in the plane perpendicular to the axis[mm^2]

The sliding speed is calculated with **(4)** (see page 57)

$$Vst = \frac{Vtr}{\text{sen}\,\alpha} = \frac{2{,}8\left[\frac{m}{min}\right]}{\text{sen}\,4°03'} \qquad Vst \cong 39{,}6\left[\frac{m}{min}\right]$$

Vtr = motion speed $\left[\frac{m}{min}\right]$
α = thread helix angle

The value of the product p • Vst is:

$$p \bullet Vst = 0{,}57\,[N/mm^2] \bullet 39{,}6\left[\frac{m}{min}\right] \cong 22{,}57\left[\frac{N}{mm^2} \bullet \frac{m}{min}\right]$$

In order to remain within the continuous working conditions, corrected by the safety factor *fi* from table N° 1, in this case =0,77, the maximum admissible value of p•Vst is **(6)** (see page 59)

$$p \bullet Vst\ am = (p \bullet Vst)_{max} \bullet fi = 21 \bullet 0{,}77\left[\frac{N}{mm^2} \bullet \frac{m}{min}\right] \qquad p \bullet Vst\ am = 16{,}15\left[\frac{N}{mm^2} \bullet \frac{m}{min}\right]$$

As the maximum admissible value of the product p•Vst is lower than the value obtained with a nut FTN 30 AR, we shall try using a nut HDL 30 AR (bronze flanged nut with 3xTr length, Tr 30x6 thread, right)

The contact surface pressure is **(1)** (see page 57)

$$p = \frac{F}{At} = \frac{1200\,[N]}{2120\,[mm^2]} = 0{,}57 \left[\frac{N}{mm^2}\right]$$

F = Axial Force [N]
At = Total bearing surface between the teeth of the screws and the nuts in the plane perpendicular to the axis[mm^2]

The sliding speed remains the same as the previous calculation

$$Vst = 39{,}6\left[\frac{m}{min}\right]$$

The value of p • Vst is now:

$$p \bullet Vst = 0{,}31\left[\frac{N}{mm^2}\right] \bullet 39{,}6\left[\frac{m}{min}\right] \cong 12{,}28\left[\frac{N}{mm^2} \bullet \frac{m}{min}\right]$$

The value obtained is now lower than the admissible one, therefore the HDL 30 AR is chosen.

Plastic Nuts sizing

In applications where silence is important or where lubrication is not allowed (grease or oil), self lubricating plastic nuts are recommended. The use of plastics is very constrained by the actual working conditions, therefore we do suggest studying the solution together with our technical office and not relying on a choice based only on intuition. This is because plastic materials have sometimes great features such as low friction and self-lubrication, but at the same time limitations caused by operating temperatures, hygroscopic problems, or some mechanical features that may not be suitable for the intended use. An advanced study of the application in this case is therefore required in order to obtain positive and satisfying results.

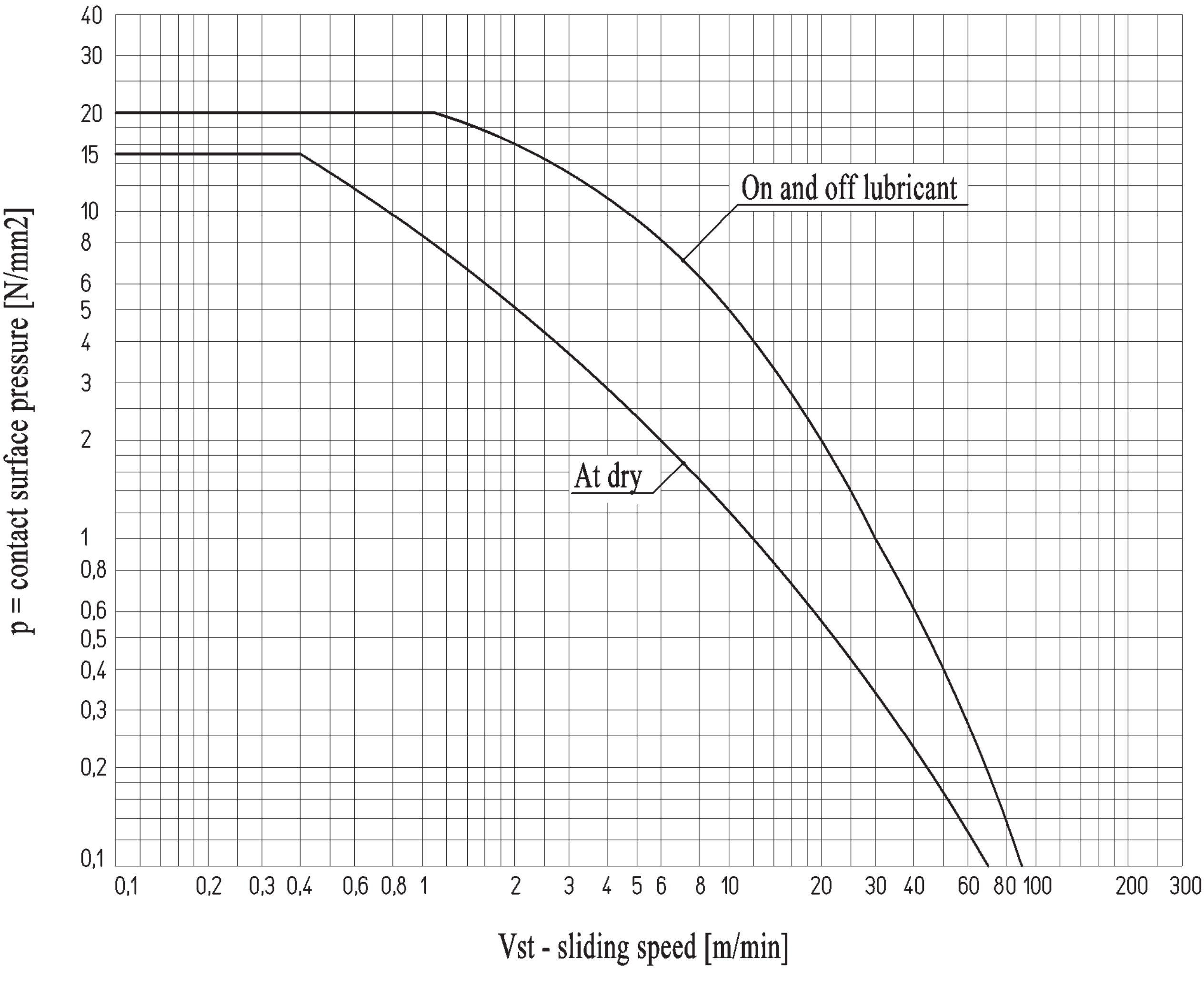
Regarding the plastic nuts, the study of the product p•Vst allows you to draw a chart which describes a curve that limits the values of p•Vst within which we have a gentle flow of the surfaces in contact with limited wearing of the nut and constant in time. Operating outside the limit drawn on the chart is not possible as in this case we would have a quick wearing of the nut due to the surface erosion caused by the contact with the screw.

Cylindrical nut MPH

Graph N° 2 shows the limit of the product p•Vst of the cylindrical nut MPH. As this plastic is resistant to wear but not self-lubricant, it's necessary to draw the limit curve relating to material used in dry conditions and intermittently lubricated material.

Graph N° 2 – Sliding condition for nuts MPH

Test condition: - continuous operation - temperature 23°C – relative humidity approx 50%



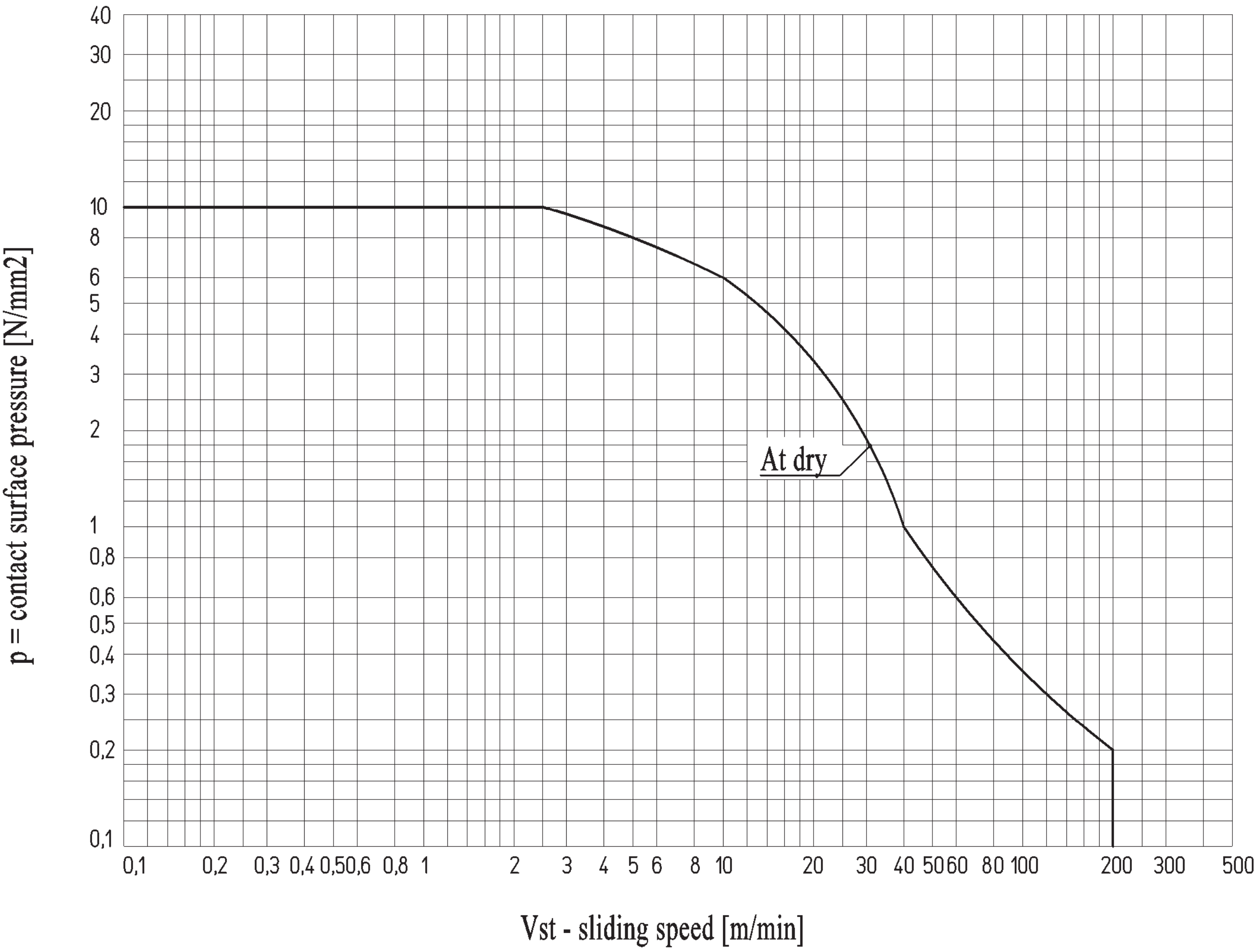
Self-lubricating plastic flanged nut with 3xTr length FCS

Graph N° 3 shows the limit of the product p•Vst of the nut FCS. The plastic used for the FCS features a strong resistance to wear and a complete self-lubricating property.

Before using the FCS, please read what stated on page 52.

Graph N° 3
Sliding conditions for nuts in self-lubricating plastic FCS

Test conditions: - continuous operation - temperature 23°C – relative humidity approx 50% with no lubrication



 We riserve the right to change sizes and features without notice.

General considerations for plastic nuts

The use of plastics is very constrained by the actual working conditions, therefore you may need to study the solution together with our technical department, and not rely on a choice based on intuition only. This is because plastics have sometimes excellent self-lubrication features, but have, at the same time, restrictions on the working temperature or humidity absorption problems as well as some mechanical properties that may not be suitable for the intended use. The preliminary study of the application, in such cases, is therefore required to achieve positive and satisfying results.

Safety factor for the forces of inertia "*f i*"

During the sizing process we must also check that the inertia forces present during acceleration and deceleration are relatively low so that the value of p●Vst remains within the controlled limits. Whereas this calculation is difficult, in the presence of a non-uniform movement or under great variations, safety factors reported in Chart. N°2 must be considered.

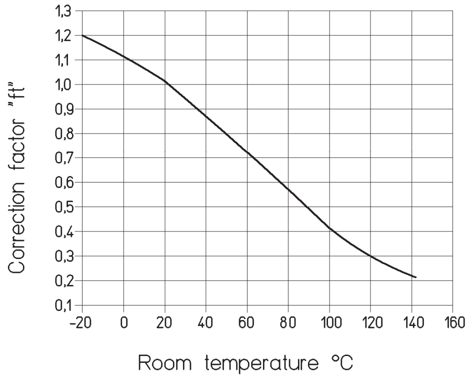
Chart. n° 2 : Safety factors with respect to the forces of inertia

Load type	*f i*
Constant loads and controlled acceleration / deceleration.	from 1 to 0,5
Constant loads and violent start and stop	from 0,5 to 0,33
Loads and speed greatly variable	from 0,33 to 0,25
Loads in presence of shocks and vibrations	from 0,25 to 0,17

Correction factor for working environment temperature

Using plastic nuts MPH o FCS, the value of p•Vst admissible must be corrected in function of the working environment temperature. Plastic becomes softer at higher temperature and withstands minor load. At lower temperatures, it becomes harder and bears heavier loads. Correction factor "*f* t" is shown in graph n° 4.

Graph N°4 - Correction factor "ft"
for nuts MPH and FCS



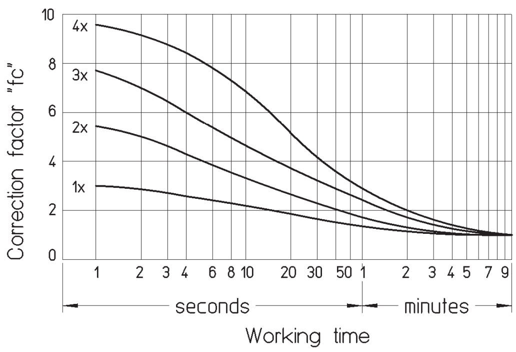
Correction factor dependent on intermittent use

Plastic nuts operating in on and off cycles for relatively short periods of time do not reach the limit of the maximum permissible temperature of the surface in contact with the screw. This temperature is a constraint that mainly contributes to limit the values of the product p•Vst in graphs N° 2 and N° 3 for the nuts MPH e FCS in continuous operation. The value of p•Vst admissible when operating in on and off cycles is higher than the value in continuous cycles. Deduce from graph N° 5 the value of the factor "*f* c". The curves of “x” represent the relationship between the downtime and the working time of the nut.

- l x represents downtime same as working time.
- 2 x represents downtime twice as much of the working time.
- 3 x represents downtime three times the working time.
- 4 x represents downtime four times the working time.

Find the working time value on the horizontal axis the working time value for the case in exam, climb vertically until intersecting the line of the relationship between the downtime and work time, then move horizontally and read the value of "*f* c".

Graph N°5 - Correction factor "fc"
for nuts MPH and FCS



The values of the three coefficients *"fi", "ft", "fc"* are used to correct the value of the product "(p•Vst)" max read from graph N° 2 (for nut MPH) or graph N° 3 (for nut FCS), considering the maximum admissible sliding speed in “test conditions” relating to the contact surface pressure value of the real case in exam.

To calculate the admissible p•Vst of the case in exam we shall use **(7) :** $p \bullet Vst\ am = (p \bullet Vst)_{max} \bullet fi \bullet ft \bullet fc$

Example of calculation with self-lubricating plastic nut

Size to wear a nut FCS flanged in self-lubricating plastic with 3xTr length which operate in the following conditions:

- Constant axial load with forces of inertia limited by controlled ramps of acceleration/deceleration of F = 1750 N
- Moving speed = 10 m / min
- Working time = 20 sec. With downtime = 60 sec.
- Working environment temperature = 50°C
- No lubricant

The nut FCS is perfectly self-lubricating and therefore suitable to operate in the considered conditions.
We choose a nut which is available among those that may be compatible with the dimensions of the motion system to be realized. Then we verify that the value of the product p•Vst is lower than the admissible value of p•Vst as per the graph N° 3 and then correct it with the coefficients "*fi*", "*ft*" and "*fc*" from the chart N° 2 and graphs N° 4 and 5.

We choose the FCS40AR (flanged nut in self-lubricating plastic with 3xTr length, Tr 40x7 right threaded)
We calculate the contact surface pressure with **(1)**

$$p = \frac{F}{At} = \frac{1750\,[N]}{6880\,[mm^2]}$$

F = Axial Force [N]
At = Total bearing surface between the teeth of the screws and the nuts in the plane perpendicular to the axis [mm^2]

$$p = 0,25 \left[\frac{N}{mm^2}\right]$$

The sliding speed is calculated with **(4)**

$$Vst = \frac{Vtr}{sen\ \alpha} = \frac{10\left[\frac{m}{min}\right]}{sen\ 3°30'}$$

Vtr = Motion Speed $\left[\frac{m}{min}\right]$
α = thread helix angle

$$Vst \cong 164 \left[\frac{m}{min}\right]$$

The value of the product p•Vst is:

$$p \bullet Vst = 0,25\,[N/mm^2] \bullet 164 \left[\frac{m}{min}\right] \cong 41 \left[\frac{N}{mm^2} \bullet \frac{m}{min}\right]$$

Now we calculate the admissible value of the product p•Vst in the conditions in exam.
From the graph N° 3 we see that in continuous working conditions at 23°C with p = 0,25 [N/mm^2] the admissible value of Vst is ≅ 140 [m/min]

i.e. $(p \bullet Vst)_{max} = 0,25 \bullet 140 = 35 \left[\frac{N}{mm^2} \bullet \frac{m}{min}\right]$

- From graph N° 2 we read the value of the coefficient "*fi*". In our case "*fi*" may be = 0,75.
- From graph N° 4 we read the value of the coefficient "*ft*". In our case, in the working environment temperature of 50°C we may assume "*ft*" = 0,8
- From graph N° 5 we read the value of the coefficient "*fc*". In our case with working time of 20 sec. and downtime of 60 sec., therefore

$$\frac{downtime}{working\ time} = 3\ (curve\ 3x)$$

we assume "*fc*" = 3,7

The maximum admissible value of the product p•Vst in our case is **(7):**

$$p \bullet Vst\ am = (p \bullet Vst)_{max} \bullet fi \bullet ft \bullet fc = 35 \left[\frac{N}{mm^2} \bullet \frac{m}{min}\right] \bullet 0,75 \bullet 0,8 \bullet 3,7 = 77,7 \left[\frac{N}{mm^2} \bullet \frac{m}{min}\right]$$

As the value of the product p•Vst in this case is lower than the admissible value, the nut FCS 40 AR may be used for this motion.

Lifetime of the plastic nut

Using the experimental values it is possible to give an indication of the lifetime a plastic nut may have. The parameters that affect the life of a plastic nut are as follows:
- Value of the contact surface pressure p [N/mm^2]
- Value of the sliding speed Vst [m/min]
- Constant of the resistance to the wear of the plastic in exam derived from experimental tests k $\left[\frac{mm3 \bullet min}{N \bullet m \bullet hrs}\right]$
- Correction factor *f*c of the on and off cycle.

All data shown below are for coupling of plastic nuts with our precision rolled screws as we guarantee a surface roughness less than 1 μm Ra.
Coupling plastic nuts with lathed screws is not possible.
The following calculations and considerations are for screws working at a temperature of approx 20/25°C with relative humidity from 30% to 70%.
For working environment at a different temperature and humidity, you should contact our Technical Office directly.

To calculate the lifetime we use the following formula:

$$t = \frac{m \bullet fc}{p \bullet Vst \bullet k} \qquad (8)$$

m = increase in the axial play between screw and nut in respect of the initial value [mm]
*f*c = correction factor from graph N° 5
p = contact surface pressure (see page 53 onward) [N/mm^2]
Vst = sliding speed (see page 53 onward) [m/min]
k = constant of resistance to wear $\left[\frac{mm3 \bullet min}{N \bullet m \bullet hrs}\right]$

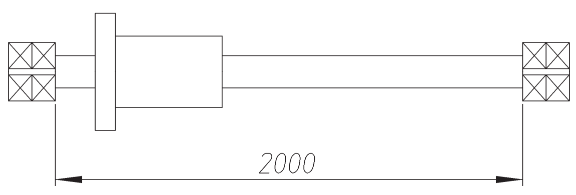
Value of the constant k for plastic nuts.

nuts MPH	$k = 10{,}5 \bullet 10^{-5}$
nuts FCS	$k = 2{,}5 \bullet 10^{-5}$

Example of lifetime calculation of a plastic nut

Size to wear and calculate the lifetime of the nut FCS operating in the following conditions:
- Constant axial load forces of inertia limited by controlled ramps of acceleration/deceleration of F = 450 N
- Motion speed = 10 m/min
- Working time = 12 sec. with downtime = 12 sec.
- Distance covered in 12 sec. at 10 m/min ≅ 2000 mm
- Working environment temperature ≅ 22°C
- Working environment mean relative humidity ≅ 40% : 60%
- No lubrication
- Minimum lifetime requested: the coupling screw/nut must work for 200.000 cycles (i.e. approx 1.330 hrs at the above conditions) increasing the axial play in respect of the initial value of 0,1 mm.

V motion =10 m/min



Nuts type FCS are perfectly self-lubricant and therefore suitable to work in the considered conditions.
Seen the good motion speed requested (10 m/min) we verify to wear the nut FCS 28 BR, with pitch 10 (2 starts at pitch 5).
To verify the product p•Vst see example on page 60.

Contact surface pressure is calculated with **(1)**.

$$p = \frac{F}{At} = \frac{450\,[N]}{3600\,[mm^2]} = 0{,}125\left[\frac{N}{mm^2}\right]$$

The sliding speed is calculated with **(4)**.

$$Vst = \frac{Vtr}{sen\,\alpha} = \frac{10\left[\frac{m}{min}\right]}{sen\,7°07'} = 80{,}7\left[\frac{m}{min}\right]$$

The value p•Vst is:

$$p \bullet Vst = 0{,}125\,[N/mm^2] \bullet 80{,}7\left[\frac{m}{min}\right] \cong 10\left[\frac{N}{mm^2} \bullet \frac{m}{min}\right]$$

Now we calculate the admissible value of the product p•Vst at the considered conditions.
From graph N° 3 we see that in continuous working conditions at 23°C with p = 0,125 [N/mm^2] the admissible value of Vst is ≅ 180 [m/min]

$$\text{i.e. } (p \bullet Vst)\,max = 0{,}125 \bullet 180 = 22{,}5\left[\frac{N}{mm^2} \bullet \frac{m}{min}\right]$$

- from chart N° 2 *"fi"* = 0,75
- form graph N° 4 " *ft"* = 1
- from graph N° 5 *"fc"* = 3

- the maximum admissible value of p•Vst, in this case, with **(7) :**

$$p \bullet Vst\,amm = p \bullet Vst \bullet fi \bullet ft \bullet fc = 22{,}5\left[\frac{N}{mm^2} \bullet \frac{m}{min}\right] \bullet 0{,}75 \bullet 1 \bullet 2 = 33{,}75\left[\frac{N}{mm^2} \bullet \frac{m}{min}\right]$$

As the value of p•Vst is here less than the admissible one, the nut FCS 28 BR may be use for this motion.

Verify to wear:

Now we calculate in how long we would face wear in continuous working conditions and therefore an increase of the axial play of 0,2 mm with **(8)**

$$t = \frac{m \bullet fc}{p \bullet Vst \bullet k} = \frac{0{,}1 \bullet 2}{10 \bullet 2{,}5 \bullet 10^{-5}} = 800 \text{ hrs}$$

Therefore 800 working hrs, at the speed of 10 m/min, correspond to the following distance:

800 • 60 • 10 = 480.000 m

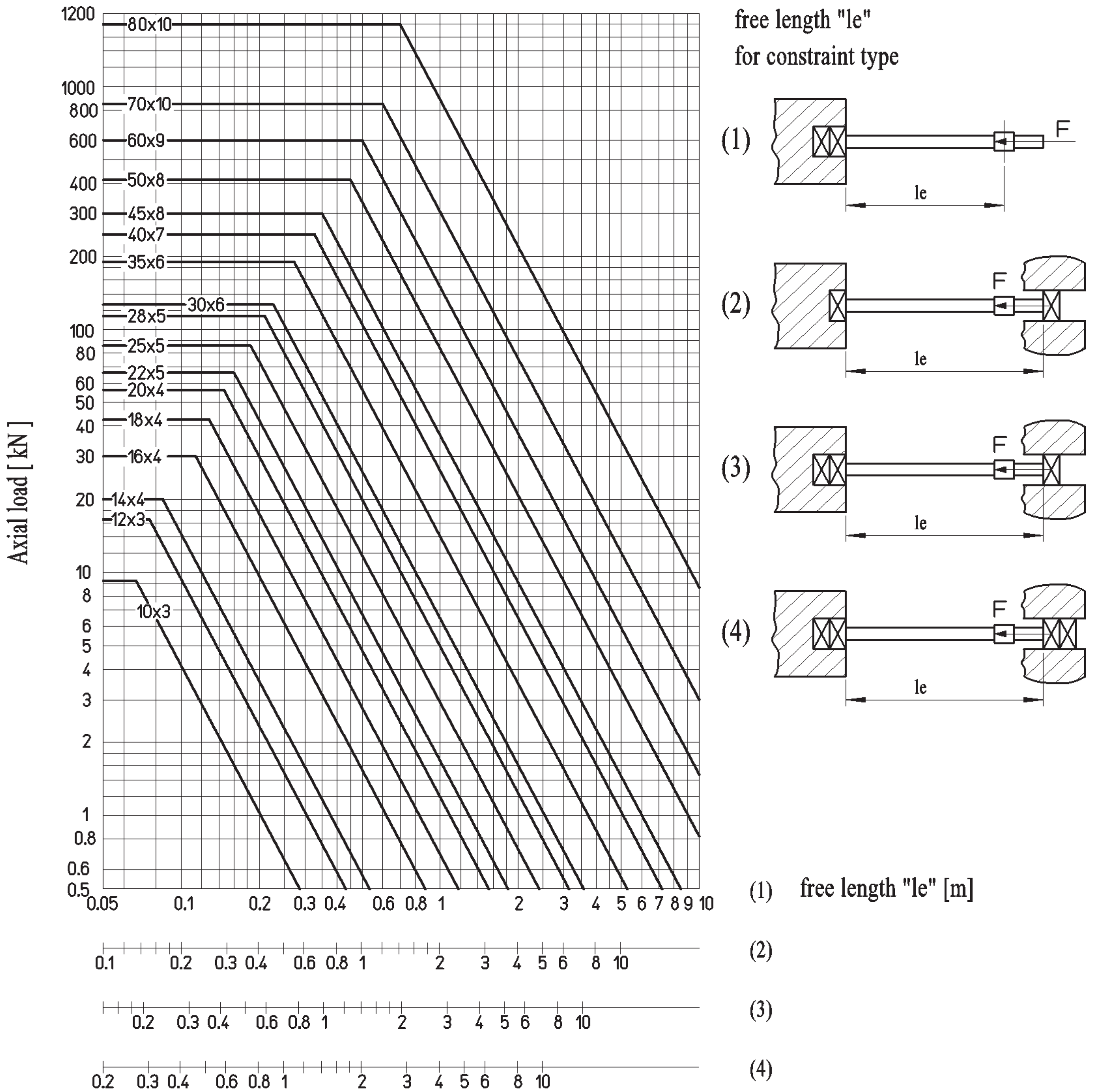
Number of cycles: $\frac{480.000}{2} = 240.000$ cycles

We have a lifetime of 1.600 hrs. at the considered conditions.

Critical Axial Load (Peak Load)

When there are compression loaded screws allowance must be made for limitations due to peak load to avoid screw bending due to excessive axial compression load. Admissible axial load depends on the core diameter (d3) of the screw, end constraints (bearings) and free length 'le'.
Regarding the values given in graph no. 6, allow a minimum safety factor ≥ 2.

Graph no. 6 - Peak Load



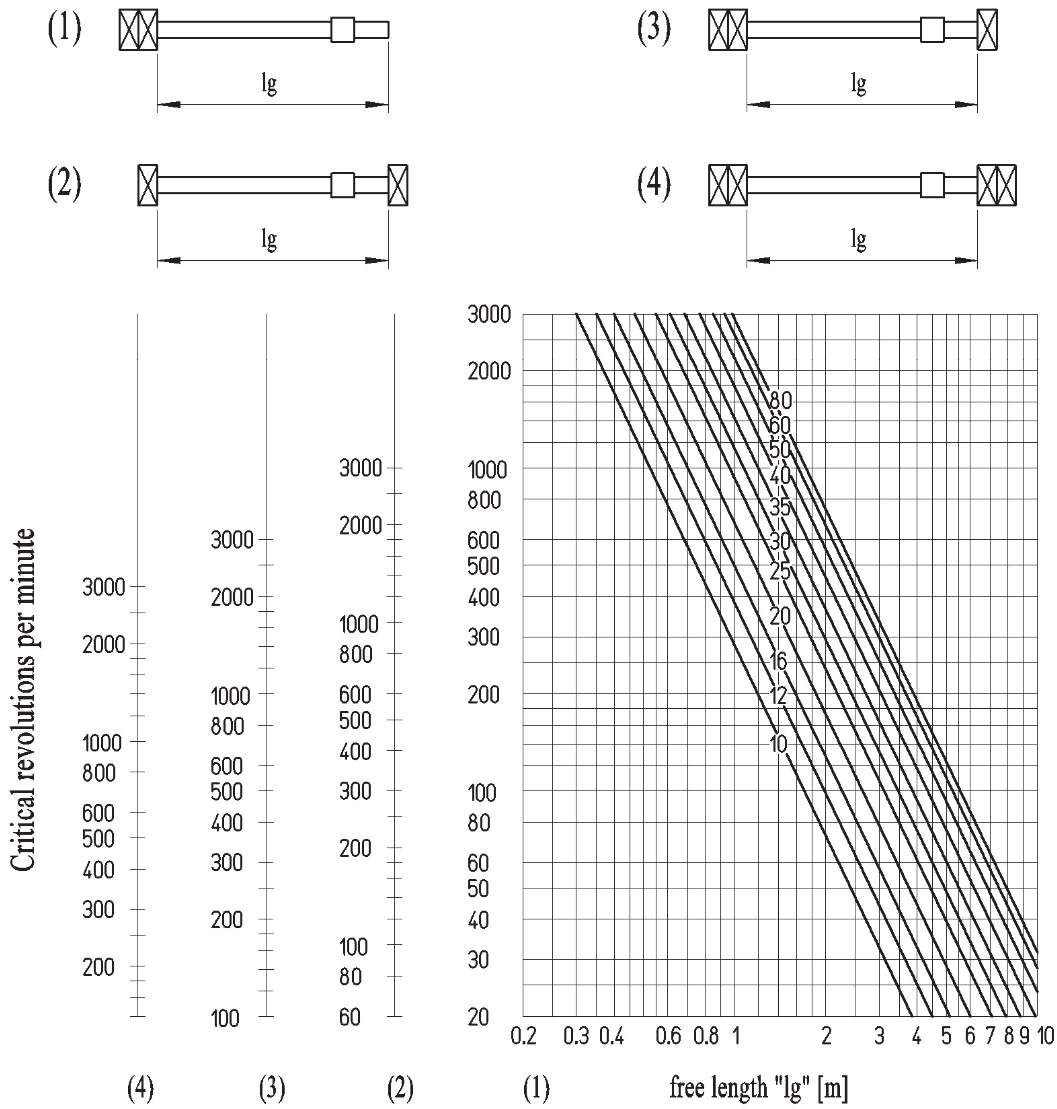
Example: find the admissible axial load of a Tr 30x6 screw 3000 mm long with constraint conditions as in drawing 4.
From graph 6 Take Fmax = 11 kN with safety factor of 2 and assume Fadm = 11/2 = 5.5 kN.

Critical revolutions per minute

The critical revolutions per minute is the rotating speed at which screw vibrations appear. This rotation speed must never be reached because the vibrations cause serious operating irregularities. Critical rpm depend on screw diameter, end constraints (bearings), free length "lg" and from the assembly accuracy.
For values shown in Graph 7 assume a minimum safety factor related to the assembly accuracy as per the following chart:

Chart n°3 Assembly accuracy coefficient:		
Assembly accuracy	**Conditions**	**Safety coefficient**
Good assembly accuracy: - Nut alignment to screw within 0.05mm	Bearing and nut seats obtained from CNC lathe onto an already finished structure.	1.3 – 1.6
Medium assembly accuracy: - Nut alignment to screw within 0.10mm	Bearing and nut seats processed on parts which are then assembled together. Alignments are checked by comparators with estreme care after mounting.	1.7 – 2.5
Low assembly accuracy: - Nut alignment to screw within 0.25mm	Bearing and nut seats processed on parts which are then assembled or welded together. Alignments are checked by comparators after mounting.	2.6 – 4.5

Graph no. 7 – Critical rpm



Example: find the critical rpm of a screw Tr 40x7 length 3000 mm with constraint conditions as in drawing 3 with average assembly accuracy. Graph 7 gives critical rotation speed ≅ 1000 rpm
From chart n°3 we calcolate the Safety coefficient = 2.2.
We can reach the working speed at a maximum round speed of: n. max = 1000/2.2 = 454 rpm.

Efficiency

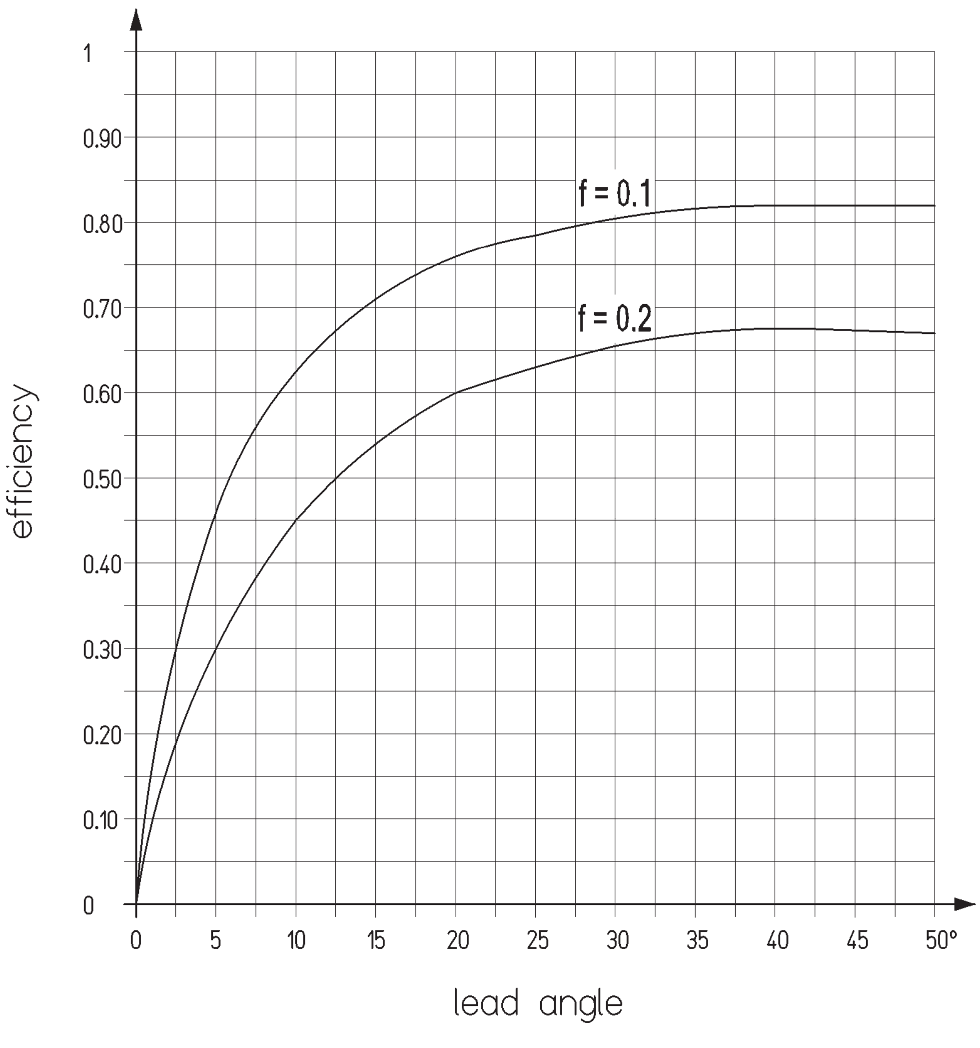
By efficiency is meant the ability of a screw & nut system to convert rotary motion into linear motion. This parameter allows appraisal of how much rotation energy is converted into useful energy for linear movement, hence how much energy is dissipated as heat.
The following formula can be used for calculation.

$$(9) \quad \eta = \frac{1 - f \bullet \mathrm{tg}\alpha}{1 + \dfrac{f}{\mathrm{tg}\alpha}}$$

η = efficiency
f = dynamic friction factor between scew and nut materials
α = lead angle of threads

The numerical efficiency values of each limit are shown in the table 'Screw Specifications' on page 54.

Graph no. 8 – Efficiency



Graph no. 8 shows that efficiency is greater if the lead angle of the screw thread is greater, hence to dissipate less energy as heat, it is recommended to use screws with lead angle as high as possible for the type of work (Pay attention if the system must be self-locking). Efficiency is inversely proportionate to the dynamic friction factor, i.e. using material with a lower friction factor there is less waste of energy. For this reason we make precision rolled trapezoidal screws with minimal roughness on the side of the tooth and always less than 1 µm Ra (usually 0.2 to 0.7 µm). We also make wear-resistant self-lubricating plastic flanged nuts which ensure very low friction factors with no need for lubrication. Dynamic friction factor $f \cong 0.1$, stiction factor $\cong 0.15$.

Torque

The Torque necessary for moving a screw & nut system is calculated by the following equation.

$$(10) \quad C = \frac{F \bullet P}{2\,\pi\,\eta\,1000}$$

C = torque (input) [N•m]
F = axial force on nut [N]
P = true lead of screw [mm]
η = efficiency (assume efficiency with stiction factor f= 0.2, Table on page 52)

Example of calculation :

Find torque necessary for movement of a screw Tr 30x6 coupled with a nut HCL Tr 30x6.

Resistant axial force = 10.000 N
Screw lead = 6 mm
$\eta = 0.26$

$$\text{Torque} = \frac{F \bullet P}{2 \bullet \pi \bullet \eta \bullet 1000} = \frac{10.000\,[N] \bullet 6\,[mm]}{2 \bullet \pi \bullet 0.26 \bullet 1000} = 36.7\ N \bullet m$$

The torque value does not consider the efficiency of mechanical parts moving together with the screw system, such as bearings, belts or other transmission components. In project phase, an increase between the 20 and 30% of the theoretical value is recommended. If electric motors with low static torque are used assume another increase of 50% to find nominal torque.

$C = 36.7\ [N \bullet m] \bullet 1.3 \bullet 1.5 \cong 71.6\ [N \bullet m]$

Power

The power necessary for moving a trapezoidal screw & nut system is calculated with the following equation.

$$(11) \quad P = \frac{C \bullet n}{9550}$$

P = power [kW]
C = torque [N•m]
n = rpm

Example of calculation :

Calculate the power necessary for moving the screw Tr 30x6 of the above example at 600 rpm.

$$P = \frac{C \bullet n}{9550} = \frac{71.6\,[N \bullet m] \bullet 600\,[round/min]}{9550} \cong 4.5\ kW$$

This is the minimum useful power necessary.

